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NP10 8QQ

I, the undersigned, being an officer duly authorised in accordance with Section 74(1) and (4) of the Deregulation and Contracting Out Act 1994, to sign and issue certificates on behalf of the Comptroller-General, hereby certify that annexed hereto is a true copy of the international application filed on 5 June 2002 under the Patent Cooperation Treaty at the UK Receiving Office. The application was allocated the number PCT/GB2002/02580

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Signed Klaylos

Dated 27 January 2003

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0	For receiving Office use only					
0-1	International Application No.	PCT/GB 02/02580				
0-2	International Filing Date	05 JUNE 2002 05-06-02				
0-3	Name of receiving Office and "PCT International Application"	United Kingdom Falent Office PCT International Application				
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0-4	Form - PCT/RO/101 PCT Request					
0-4-1	Prepared using	PCT-EASY Version 2.92 (updated 01.01.2002)				
0-5	Petition					
	The undersigned requests that the present international application be processed according to the Patent Cooperation Treaty					
0-6	Receiving Office (specified by the applicant)	United Kingdom Patent Office (RO/GB)				
0-7	Applicant's or agent's file reference	N01/0301/PCT				
1	Title of invention	FLOW MEANS				
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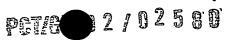
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Name(s) LAWRENCE, John, Gordon; COLLINGS Anthony, Robert; LAMBERT, Ian, I ROBERTSON, James, Alexander; MCG Graeme, David	CALLUM, CZ UG ZM a Protocol and any ng State on and of CR GB GR other te of and of W ML MR which is tracting
ROBERTSON, James, Alexander; MCG Graeme, David V Designation of States V-1 Regional Patent (Other kinds of protection or treatment if any, are specified between parentheses after the designation(s) concerned) AP: GH GM KE LS MW MZ SD SL SZ ZW and any other State which is Contracting State of the Harare and of the PCT EA: AM AZ BY KG KZ MD RU TJ TM and other State which is a Contract: of the Eurasian Patent Convention the PCT EP: AT BE CH&LI CY DE DK ES FI IN ITE IT LU MC NL PT SE TR and any State which is a Contracting State wh	ZZ UG ZM a Protocol and any ang State on and of CR GB GR other ate of and of W ML MR which is tracting
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V-5 Precautionary Designation Statement	
In addition to the designations made under items V-1, V-2 and V-3, the applicant also makes under Rule 4.9(b) all designations which would be	
permitted under the PCT except any designation(s) of the State(s) indicated under item V-6 below. The applicant	
declares that those additional designations are subject to confirmation	
and that any designation which is not	
confirmed before the expiration of 15 months from the priority date is to be	
regarded as withdrawn by the applicant	
at the expiration of that time limit. V-6 Exclusion(s) from precautionary NONE	
designations	



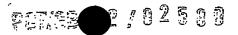
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VI-1	Priority claim of earlier national	,	
VI-1-1	application Filing date	05 June 2001 (05.06.200	1.)
VI-1-2	Number	0113633.2	- /
VI-1-3	Country	GB	
VI-2	Priority document request		
	The receiving Office is requested to prepare and transmit to the International Bureau a certified copy of the earlier application(s) identified above as item(s):	VI-1	
VII-1	International Searching Authority Chosen	European Patent Office	(EPO) (ISA/EP)
VIII	Declarations	Number of declarations	
VIII-1	Declaration as to the identity of the inventor	-	
VIII-2	Declaration as to the applicant's entitlement, as at the international filing date, to apply for and be granted a patent	-	
VIII-3	Declaration as to the applicant's entitlement, as at the international filing date, to claim the priority of the earlier application	-	
VIII-4	Declaration of inventorship (only for the purposes of the designation of the United States of America)	-	
VIII-5	Declaration as to non-prejudicial disclosures or exceptions to lack of novelty	-	
IX	Check list	number of sheets	electronic file(s) attached
IX-1	Request (including declaration sheets)	6 -	
IX-2	Description	12 -	
IX-3	Claims	4	
IX-4	Abstract	1 EZZ	ABST00.TXT
IX-5	Drawings	4 -	
IX-7	TOTAL	27	
	Accompanying items	paper document(s) attached	electronic file(s) attached
IX-8	Fee calculation sheet	√	
IX-17	PCT-EASY diskette	- Dis	kette
IX-19	Figure of the drawings which should accompany the abstract	2	
IX-20	Language of filing of the international application	English	
X-1	Signature of applicant, agent or common representative	mmm	
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10-1	Date of actual receipt of the	115	JUNE	2002	05-01 00
	purported international application	@ M	66117PP		03.00-02





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10-2	Drawings:	
10-2-1	Received	·
10-2-2	Not received	<u>-</u>
10-3	Corrected date of actual receipt due to later but timely received papers or drawings completing the purported international application	
10-4	Date of timely receipt of the required corrections under PCT Article 11(2)	·
10-5	International Searching Authority	ISA/EP
10-6	Transmittal of search copy delayed until search fee is paid	

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ME 02/02523 T/CD 02/02560

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PCT-EASY INFORMATION SHEET

(For applicant use only, DO NOT submit this sheet with the international application)

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	Contents
Yellow!	The power of attorney or a copy of the general power of attorney will need to be furnished unless all applicants sign
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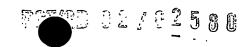
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- -Box X of the Request form has been signed:
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Flow Means



There is a disclosed a conduit supporting structure that imposes, maintains and/or reinforces a flow guiding rmation of a conduit, whereby to effect a desired flow configuration in the conduit.

Flow means

This invention relates to means for effecting fluid flow patterns in conduits, particularly but not exclusively conduits such as blood flow tubing and stents, and other tubing carrying fluids essential to life or industrial fluids.

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WO00/38591 discloses conduits such as tubing and stents devised to induce helical flow in such a fashion as to eliminate or reduce turbulence and/or eliminate or reduce dead flow regions in the conduits. The conduit has internal helical grooving or ridging or other measures which induce such helical flow, taking into account the conduit dimensions and the viscosity and velocity of fluid.

External structures have been used to provide reinforcement of conduits (see for example US3479670 and US4130904), which may serve to protect the conduits from kinking or maintain conduits in an open positions but do not directly influence internal geometry of the conduit lumen. For example, in US3479670 the tube lumen remains smooth despite the presence of reinforcing polypropylene monofilaments wrapped around the tube.

In accordance with a first aspect of the present invention there is provided a conduit, adapted for flow of a fluid having characteristics and velocity and having a given diameter, by apparatus that imposes, maintains or reinforces a flow guiding formation internally of the conduit, the apparatus comprising a helical structure to cause helical, rotational flow eliminating or reducing turbulence and/or eliminating or reducing dead flow regions in the flow, when used for such a fluid flow.

In accordance with a second aspect of the invention, there is provided apparatus for forming a helical flow formation in a conduit, the apparatus comprising a helical structure, and

being adapted to be engaged with a conduit for carrying a fluid, in use, such that the helical structure forms the helical flow formation inside the conduit, the angle of the helical flow formation being determined from the internal dimensions of the conduit, the fluid mass flow of the conduit, the pressure drop along the conduit and the turbulent kinetic energy within the conduit.

In accordance with a third aspect of the present invention, there is provided a method of determing the helix angle of a helical flow formation within a conduit, the method comprising specifying the internal dimensions of the conduit and an intended fluid mass flow through the conduit, and determing the helix angle from the pressure drop and the turbulent kinetic energy for a conduit having the specified internal dimensions and intended fluid mass flow.

Typically, the pressure drop and the turbulent kinetic energy are non-dimensionalised before the helix angle is determined.

Preferably, the helix angle is determined as the helix angle at which the non-dimensionalised pressure drop and the non-dimensionalised turbulent kinetic energy are substantially equal.

The helical flow formation may have a helix angle of between 5° and 50°. For example, the helical flow formation may have a helix angle of about 8°, particularly but not exclusively in relation to arterial flow in leg arterial grafts.

Typically, the fluid to be carried by the conduit comprises a liquid. The fluid may be a solely a liquid, a liquid mixed with a particulate solid, or a liquified solid. For example, where the conduit is blood vessel, the liquid is blood.

Preferably, the side wall of the conduit is deformable and the apparatus is engaged with the external side wall of the conduit such that the helical structure deforms the side wall of the conduit to form the helical flow formation on the interior of the conduit.

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The helical flow formation may effect a rotational flow. The rotational flow may comprise a helical and/or spiral flow component.

The helical structure may comprise ridges which define a specific profile of the helical flow formation which effects the fluid flow pattern. Additionally or alternatively, the helical structure may comprise grooves which define a specific profile of the helical flow formation which effects the fluid flow pattern.

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The helical flow formation may be orientated with a Z twist. A Z-twist orientation (also referred to as a right hand helix) creates clock-wise flow-inducing in the forward flow direction. Alternatively, the helical flow formation may be orientated with an S twist (also referred to as a left hand helix).

The apparatus may comprise symmetrical protrusions and/or asymmetrical protrusions, the asymmetrical protrusions having a gradually sloping leading edge and a steep sloping rear edge.

The apparatus may comprise single-start or multistart grooving and/or ridging.

The apparatus may comprise a frame. The frame may be formed by circular, rectangular, ovoid and/or differently parts. The frame may comprise parts having at least two different diameters.

The apparatus may comprise metals such as stainless steel. Alternatively or additionally, the structure may comprise synthetic or other thermoplastic or plastifiable material, being plastified and reset in twisted condition. Suitable materials include polytetrafluoroethylene (PTFE, also known as "Teflon"), polypropylene, nylon or other synthetic material.

-4-

Stainless steel or other metallic structures may be coated with synthetic or other thermoplastic or plastifiable material.

The apparatus may have a twisted appearance with an oval, rectangular or other non-circular cross-section. The structure may be coiled along its longitudinal axis and have a circular cross-section.

The apparatus may comprise patterned or solid material. The structure may be fixed or collapsable.

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The helical flow formation may effect helical and/or spiral flow in such a fashion as to eliminate or reduce turbulence and/or eliminate or reduce dead flow regions in the conduit. Optimal helical angle to achieve such flow will depend on such factors as diameter of the conduit, longitudinal and rotational velocity of the fluid, and the viscosity and other characteristics of the fluid.

The apparatus may be branched.

The conduit may comprise tubing. For example, the conduit may comprise artificial or natural blood flow tubing, such as a graft or blood vessel, respectively. The tubing may be used in blood treatment or delivery equipment, for example a heat-lung machine, dialysis equipment or a giving set. The tubing may also be used in industrial equipment, for example hoses, pipes or fire hoses.

Alternatively, the conduit may comprise a stent. Stents, for example made of mesh, expanded sheet or tube or wire spring type, are inserted into blood vessels to provide mechanical support and prevent collapse of the blood vessel. A structure according to the

present invention could be placed inside or outside the blood vessel to impose, maintain and/or reinforce a flow guiding formation through the blood vessel.

The invention may also be utilised for stent grafts, ie. a combination of stent and graft.

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Also provided according to the present invention is a method for imposing, maintaining and/or reinforcing a helical flow formation which effects a desired flow configuration in a conduit, comprising fitting a support structure around the conduit wherein the structure imposes, maintains and/or reinforces the flow guiding formation.

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Flow configuration through a conduit may, in general, be measured using such techniques MRI (magnetic resonance imaging) and/or Döppler ultrasound, and the flow guiding formation may be modified accordingly until a desired flow configuration is achieved. Initial design of flow configuration may be by mathematical modelling or by trial and error, with modification as described above.

Examples of apparatus in accordance with the invention will now be described with reference to the accompanying drawings, in which:

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Figure 1 is a perspective view of a plastics frame suitable for imposing a helical fluid flow;

Figure 2 is a perspective view of a frame as shown in Fig. 1 enclosing a graft; Figure 3 is a perspective view of support structure with a spiralling ribbon conformation;

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Figure 4A is a perspective view of a wire mesh structure with a barley twist conformation enclosing a graft;

Figure 4B shows the rotational effect of the structure depicted in Figure 4A, as viewed in the direction of arrow A in Figure 4A;

Figure 5 is a perspective view of a mesh structure coiled along its longitudinal axis and having a circular cross-section;

Figure 6 is a perspective view a scaffold comprising French knitted Nitinol; Figure 7A is a perspective view of a mesh structure comprising wires with two different diameters;

Figure 7B is a cross sectional view through line A-A' in Figure 7A;

Figure 8A is a cross-sectional view showing a method of construction of a structure;

Figure 8B is a perspective view of structure made according to the method shown in Figure 8A;

Figure 9A is a perspective view of a plate with strips, for use in the manufacture of a structure;

Figure 9B is a perspective view of a structure made using the plate shown in Figure 9A;

Figure 10A is a perspective view of a plate having a raised spline, for use in the manufacture of a structure;

Figure 10B is a perspective view of a structure made using the plate shown in Figure 10A; and

Figure 11 is a graph of helix angle versus pressure drop and helix angle versus turbulent kinetic energy for an arterial blood vessel.

The invention in general provides means and method for supporting precise internal surface architecture and configuration to induce a flow conformation, for example helical or rotational flow, thereby to improve fluid flow and reduce turbulence. Embodiments of structures encompassed by the present invention, and methods of manufacture thereof, are described below, although the invention is not intended to be limited by these examples. While the examples shown in certain cases relate to grafts or stent, the principles embodied therein also apply to other types of conduit.

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Figure 1 shows a helix structure 100 comprising ribs 1a-c which are disposed in a helical flow guiding formation along the longitudinal axis of the structure 100. Helix structure 100 further has smaller frame components (for example, connection 2) which support the orientation of the ribs 1a-c. Ribs 1a-c are more or less triangular in shape, with one of the edges of the triangle always facing the interior of the helix structure 100. With helix structure 100 is fitted over a graft 3, as shown generally at 200 in Figure 2, ribs 1a-c impose groove formations 4a-c within the lumen of the graft 3, thereby effecting the helical flow guiding formation of the helix structure 100 with the graft 3.

In a preferred embodiment, helix structure 100 comprises polypropylene, but other synthetic material, metal and/or tissue engineered material may also be used. Graft 3 comprises PTFE material, which is sufficiently malleable to be shaped by ribs 1a-c. Other medical grade plastics or plastifiable material which has this malleable characteristic, for example Dacron, may also be used for graft 3.

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Figure 3 shows a spiralling ribbon support structure 5. This structure, when fitted over a conduit, imposes or supports a double-barrelled helical flow pattern within the conduit. The helical flow pattern is effected by spiral orientation in the longitudinal axis of the structure.

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Shown generally at 300 in Figure 4A is a barley twist conformation wire mesh 6 fitted over part of the length of a graft 3. In cross-section, mesh 6 imposes on graft 3 a shape which is approximately triangular. However, when viewed through one end in the direction of arrow A, as shown in Figure 4B, graft 3 has a flow path with is circular through longitudinal axis (compacted view of circular path shown at 8) through sequential twisting of the approximately triangular cross-section shape of graft 3 (for example at stages 9 and 10). The mesh 6 thus imposes a helical flow pattern through graft 3 where mesh 6 is positioned over graft 3.

Thus a helical flow path can be induced within a conduit by means of the conformation imposed by a structure along its longitudinal axis. Another example is shown in Figure 5: longitudinally coiled mesh structure 11 has a circular cross-section throughout is conformed to induce upon a conduit within it a helical flow pattern. Grooves or ridges in the structure are not necessary to achieve the helical flow pattern in the example shown in Figure 5.

A French knitted Nitinol scaffold 6 is shown in Figure 6. Cycling the pins in the manufacturing die results in the spiral knitted sock-like conformation of the scaffold 6. The scaffold is preferably manufactured from moulded polypropylene which is injected onto a Dacron graft with a heat sealing step to bond the plastic to the graft. The scaffold can also be manufactured from nylon. The scaffold can alternatively be manufactured as a dripcast or extruded synthetic frame.

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The scaffold would be applied or compressed over a conduit, such as a graft of other blood flow tubing, to impose, maintain and/or reinforce a helical flow guiding formation within the conduit.

In another embodiment depicted in Figure 7A, a cylindrical wire mesh structure 400 comprises flow guidance forming wires 13a-c interspersed with support wires 14a,b which are orientated in the same direction and more or less parallel to the nearest flow guidance forming wire 13a-c. A flow guidance forming wire 13a-c would generally be thicker and more rigid than support wires 14a,b. When the cylindrical wire mesh structure 400 is fitted over a conduit, shown in conduit outline 15 in Figure 7B, each flow guidance forming wire 13a-c imposes a ridge within the lumen of the conduit. It may be desirable that (smaller) ridges are also formed by support wires 14a,b within the conduit enclosed by the wire mesh structure 400 - this would be dependent largely on the malleability of the conduit.

In modifications of the cylindrical wire mesh structure 400 shown in Figure 7A, the wires need not be cylindrical but may be ovoid, rectangular, square, flat or other shapes. Wires used in wire mesh structures may be metallic or non-metallic and may also be coated. In the example shown in Figure 7, there are three flow guidance forming wires 13a-c. However, the number of flow-inducing wires in this type of mesh structure may be one, two or more.

In yet another variation of the structure shown in Figure 7, the material (metal, synthetic material, etc.) of different size and/or shape can be weaved and/or braided to form a conduit such that flow guidance forming patterns are formed within the conduit by the weaved or braided material. Here, the flow guidance forming patterns may be an integral component of the conduit, rather than external to the conduit. External structures may further be imposed over such weaved/braided conduits to support, enhance and/or form alternative flow guidance patterns within the conduit.

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Further examples of structures according to the present invention and their method of manufacture are shown in Figures 8-10. Figure 8A shows in cross-section a modification 500 of a pre-formed Nitinol cylindrical mesh 16 by imposing a clamp 17 onto the Nitinol cylindrical mesh 16 in the direction of arrow 18 to create three grooves (with or without a thermal memory induction step). Figure 8B depicts the Nitinol cylindrical mesh 16 after modification 500, where each groove 18 is orientated in a helical conformation around the Nitinol cylindrical mesh 16. The modified structure 600 can be fitted over a conduit to impose, maintain and/or reinforce a helical flow configuration. The Nitinol cylindrical mesh 16 may be alternatively be a Nitinol cut tube or a stainless steel cut tube.

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An alternative method of construction of a structure is shown in Figures 9A and 9B. Here, a plate 23 has rectangular bars 24 moulded, punched or attached thereto in a specific orientation (Figure 9A). The plate 23 is rolled into a cylinder to form a ribbed cylinder 25

wherein the bars 24 form flow guiding profiles which, when the ribbed cylinder 25 is fitted over a conduit, impose, maintain and/or reinforce a flow guiding formation in the lumen of the conduit.

Figure 10A shows a Nitinol strip 26 with a raised spline 27. When the Nitinol strip 26 is rolled into a cylinder conformation, as shown in Figure 10B, spline 27 forms a flow guiding profile in the interior of the splined cylinder 28. Note that the rolled edges of splined cylinder 28 are not completely joined, which may be desirable for facilitating release or removal of the structure from a conduit. Naturally, alternative materials other than Nitinol will be amenable to these methods for forming structures according to the invention.

Structures according to the present invention can impose, maintain and/or reinforce a flow guiding formation of a conduit in a temporal manner, for example during pulsate blood flow through a blood flow tubing. The structures may be placed over natural ("native") blood vessels such as arteries or veins to impose, maintain and/or reinforce a flow guiding formation *in situ* as the blood vessel dilates. In certain cases, use of artificial grafts may be avoided. The structures may also be placed over previously implanted grafts or conduits to impose, maintain and/or reinforce a flow guiding formation.

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The choice of the helix angle of the helical flow formation is important in minimising turbulent flow and dead spots within the flow. The inventors have found that for a conduit having a given internal dimensions and a partcular helical flow formation that is intended to carry a given mass flow, the optimum helix angle can be determined from the pressure drop along the conduit and the turbulent kinetic energy in the conduit.

The inventors have found that in order to maintain a give mass flow in a given conduit, with a particular helical flow formation, the pressure drop increases as the helix angle

increases and the turbulent kinetic energy decreases as the helix angle increases. Hence, the choice of helix angle is a compromise between minimising pressure drop and minimising turbulent kinetic energy. If the pressure drop and turbulent kinetic energy are non-dimensionalised using conevntional mathematical techniques, the curves of helix angle versus non-dimensionalised pressure drop and helix angle versus turbulent kinetic energy can be plotted on the same graph. A curve 50 of helix angle versus non-dimensionalised pressure drop and a curve 51 of helix angle versus non-dimensionalised turbulent kinetic energy for an arterial graft are shown in Figure 11. These curves 50, 51 were obtained from measuring pressure drop and turbulent kinetic energy in the arterial graft using conventional techniques. The curves 50, 51 show that at the region 52, the curves intersect and this intersection occurs at a helix angle of approximately 8°.

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By also analysing flow in the graft using conventional magnetic resonance imaging techniques it was found by trial and error that the optimum helix angle for the graft for the given mass flow was also approximately 8°. Hence, the optimum helix angle for the graft occurs at approximately when the non-dimensionalised pressure drop is approximately equal to the non-dimensionalised turbulent kinetic energy.

Although in the example described above the helix angle is determined as the angle at which the non-dimensionalised pressure drop and turbulent kinetic energy are substantially equal, there may be situations in which the helix angle is selected so that the non-dimensionalised pressure drop and turbulent kinetic energy are not equal. This may situation may arise if, for example, a lower turbulent kinetic energy is required and it is decided to tolerate a higher pressure drop to obtain a lower turbulent kinetic energy. Simlarly, if a low pressure drop is more important than turbulent kinetic energy, a higher turbulent kinetic energy may be tolerated to obtain a lower pressure drop. Hence, the choice of the helix angle can be chosen according to the particular application, and different applications may have different requirements.

The present invention is also suitable for industrial applications. Structures may be imposed upon conduits such as tubes to create improved efficiency through quicker transfer of fluid and reduced energy use or a reduction in pressure gradient along the tube allowing lower pressures within the tube to deliver a specific end conduit pressure/flow rate. Structures could effect a reduction in turbulence, thereby reducing vibration, noise, and/or fatigue in a conduit, which in pumps could allow for reduced pump power consumption. Structures may allow further penetration or more accurate distribution patterns of fluid exiting a conduit, for example from a hose pipe for domestic use or from a fire hose. The invention will also be of benefit to industries where slurries or suspensions are transported through conduits, for example food producers or distributors involved with soups, sauces and like products.

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As with the example above of the graft, the optimum helix angle for these other types of conduits can be determined from the pressure drop and the turbulent kinetic energy. Therefore, the invention has the advantage of enabling the helix angle of a helical flow formation in a given size of conduit intended to carry a given fluid to be determined from the pressure drop and the turbulent kinetic energy in the conduit.

Claims

1. Apparatus that imposes, maintains and/or reinforces a flow guiding formation of a conduit, whereby to effect a desired flow configuration in the conduit.

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2. Apparatus for forming a helical flow formation in a conduit, the apparatus comprising a helical structure, and being adapted to be engaged with a conduit for carrying a fluid, in use, such that the helical structure forms the helical flow formation inside the conduit, the angle of the helical flow formation being determined from the internal dimensions of the conduit, the fluid mass flow of the conduit, the pressure drop along the conduit and the turbulent kinetic energy within the conduit.

3. Apparatus according to claim 2, wherein the helix angle is determined from the non-dimensionalised pressure drop and the non-dimensionalised turbulent kinetic energy.

4. Apparatus according to claim 3, wherein the helix angle is determined as the angle at which the non-dimensionalised pressure drop is substantially equal to the non-dimensionalised turbulent kinetic energy.

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- 5. Apparatus according to any of the preceding claims, wherein the apparatus is external of the conduit.
- 6. Apparatus according to any of the preceding claims, comprising ridges which define a specific profile of the flow guiding formation which effects the fluid flow pattern.
 - 7. Apparatus according to any of the preceding claims, comprising grooves which define a specific profile of the flow guiding formation which effects the fluid flow pattern.

- 8. Apparatus according to any of the preceding claims, wherein the flow guiding formation being orientated with a Z twist.
- 9. Apparatus according to any of the preceding claims, wherein the flow guiding5 formation being orientated with an S twist.
 - 10. Apparatus according to any of the preceding claims, comprising symmetrical protrusions and/or asymmetrical protrusions, the asymmetrical protrusions having a gradually sloping leading edge and a steep sloping rear edge.
 - 11. Apparatus according to any of the preceding claims, comprising single-start or multistart grooving and/or ridging.

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- 12. Apparatus according to any of the preceding claims, comprising a frame.
- 13. Apparatus according to claim 12, wherein the frame is formed by circular, rectangular, ovoid and/or differently shaped parts.
- 14. Apparatus according to claim 12 or claim 13, wherein the frame comprises parts having at least two different diameters.
 - 15. Apparatus according to any of the preceding claims, comprising stainless steel.
- 25 16. Apparatus according to any of the preceding claims, comprising synthetic or other thermoplastic or plastifiable material, being plastified and reset in twisted condition.

- 17. Apparatus according to any of the preceding claims, having a twisted appearance with an oval, rectangular or other non-circular cross-section.
- 18. Apparatus according to any of claims 1 to 16, being coiled along its longitudinal axis and having a circular cross-section.
 - 19. Apparatus according to any one of claims 1 to 11 or 15 to 18, comprising patterned or solid material.
- 10 20. Apparatus according to any of the preceding claims, being fixed or collapsable.
 - 21. Apparatus according to any of the preceding claims, being branched.
- 15 22. Apparatus according to any of the preceding claims, wherein the conduit comprises tubing.
 - 23. Apparatus according to claim 22, wherein the conduit comprises artificial or natural blood flow tubing.
 - Apparatus according to any one claims 1-23, wherein the conduit comprises a stent.

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25. A method for imposing, maintaining and/or reinforcing a flow guiding formation which effects a desired flow configuration in a conduit, comprising fitting a support structure around the conduit wherein the structure imposes, maintains and/or reinforces the flow guiding formation.

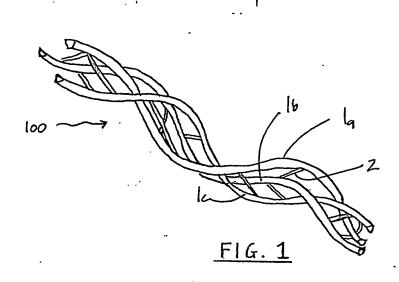
A method of determing the helix angle of a helical flow formation within a conduit, the method comprising specifying the internal dimensions of the conduit and an intended fluid mass flow through the conduit, and determing the helix angle from the pressure drop and the turbulent kinetic energy for a conduit having the specified internal dimensions and intended fluid mass flow.

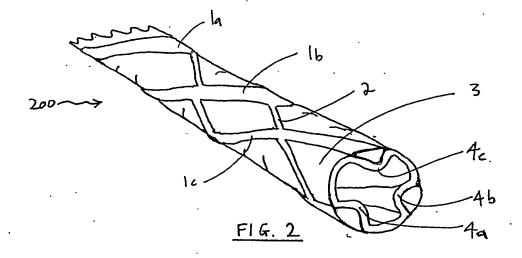
- 27. A method according to claim 26, wherein the pressure drop and the turbulent kinetic energy are non-dimensionalised before the helix angle is determined.
- 10 28. A method according to claim 27, wherein the helix angle is determined as the helix angle at which the non-dimensionalised pressure drop and the non-dimensionalised turbulent kinetic energy are substantially equal.
- 29. A method for defining and/or reinforcing a flow guidance arrangement for a conduit, comprising fitting a support structure external of the arrangement wherein the structure defines and/or reinforces the fluid flow pattern of the arrangement.

ABSTRACT

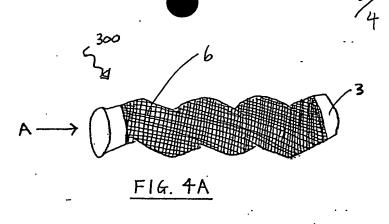
Flow Means

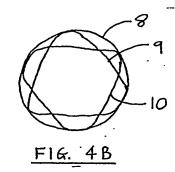
There is a disclosed a conduit supporting structure that imposes, maintains and/or reinforces a flow guiding formation of a conduit, whereby to effect a desired flow configuration in the conduit.

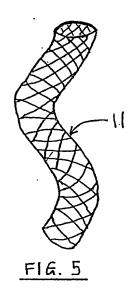


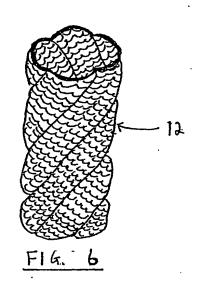


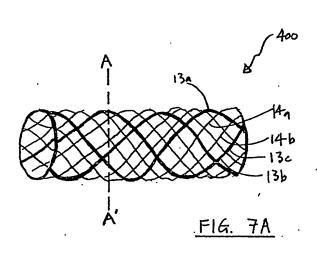
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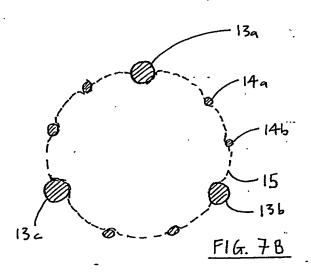


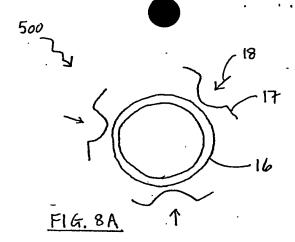


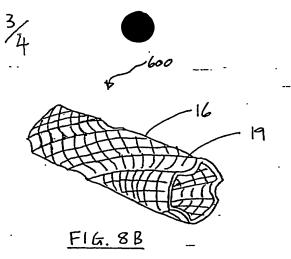


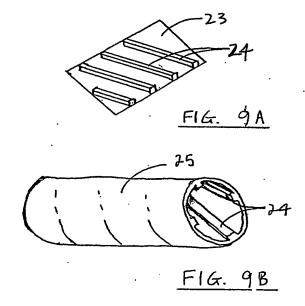


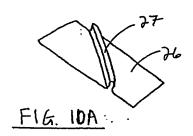


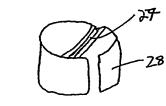












FIGIOB

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-n-non dimensional dp

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